

#### Programmable Metasurfaces for Wireless Communications: A Loaded Thin Wire Model

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# What is a **Programmable Metasurface?**



M. Di Renzo et al. Smart radio environments empowered by reconfigurable intelligent surfaces: How it works, state of research, and the road ahead. IEEE JSAC, Nov. 2020.

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### **Towards Smart Radio Environments**

### Smart (Reconfigurable) Radio Environment





#### Main features (RIS):

- No power amplifiers
- No digital signal processing
- No radio frequency chains

#### Main features (HoloS):

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- Power amplifiers
- Digital signal processing
- Radio frequency chains

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### Programmable Metasurfaces (RIS)



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RIS Example: Reflecting Metasurface

#### Reflecting Metasurface (RIS)



### **Generalized Snell's Law**

#### **Generalized Snell's Law**



$$n_{\rm t}\sin(\theta_{\rm t}) - n_{\rm i}\sin(\theta_{\rm i}) = \frac{1}{k_0}\frac{\mathrm{d}\Phi}{\mathrm{d}x}$$

$$\sin(\theta_{\rm r}) - \sin(\theta_{\rm i}) = \frac{1}{n_{\rm i}k_0} \frac{\mathrm{d}\Phi}{\mathrm{d}x}$$

Proof: Fermat's Principle (1657) "Light propagates from one point to another on trajectories such that the travel time is minimized" Generalized Snell's Law: How About the Reflected Power?





**RIS/HoloS: Rethinking the Communication Model** 

### From Plane Waves for Spherical Waves

- Paradigm #1: The wavefronts of the electromagnetic waves are (approximated as) locally planar on the antenna arrays
  - RISs/HoloS are electrically large and the transmission distances are shrinking



### **Densification of Radiating Elements**

- □ Paradigm #2: The radiating elements of antenna-arrays are decoupled electromagnetically
  - **D** The inter-distances are smaller than the wavelength ( $< \lambda/2$ )



### RIS: A Loaded Thin Wire Model

### **RIS:** A Loaded Thin Wire Model

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- □ M. Di Renzo et al. "MIMO interference channels assisted by reconfigurable intelligent surfaces: Mutual coupling aware sum-rate optimization based on a mutual impedance channel model", IEEE WCL 2021.
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## **Modeling in Free Space**

### E2E Communication Model in Free Space



# **Discrete Dipole Approximation**

M. Johnson, P. Bowen, N. Kundtz, and A. Bily, "Discrete-dipole approximation model for control and optimization of a holographic metamaterial antenna", Appl. Opt., vol. 53, pp. 5791-5799, 2014.

### E2E Communication Model in Free Space



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□ Boundary conditions (SISO case)

$$E_{qT}\left(z+z_{q}\right)+E_{qR}\left(z+z_{q}\right)+\sum_{n=1}^{N}E_{qSn}\left(z+z_{q}\right)=-V_{q}\left(z_{q}\right)\delta(z)$$

□ Boundary conditions (SISO case)

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□ Voltages at the ports of the thin wire dipoles

Transmiter: 
$$V_G(z_T) - Z_G I_T(z_T) = V_T(z_T)$$
  
Receiver:  $-Z_R I_R(z_R) = V_R(z_R)$   
RIS:  $-Z_S I_S(z_S) = V_S(z_S), \quad S = \{S1, S2, ..., SN\}$ 

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RIS:  $-Z_S I_S(z_S) = V_S(z_S), \quad S = \{S1, S2, ..., SN\}$ 

□ Projection of the field on the currents and integration

□ A system of linear equations (2 RIS elements for simplicity)

□ A system of linear equations (2 RIS elements for simplicity)  $Z_{TT}I_{T}(z_{T}) + Z_{TR}I_{R}(z_{R}) + Z_{TS1}I_{S1}(z_{S1}) + Z_{TS2}I_{S2}(z_{S2}) = V_{T}(z_{T}) = V_{G}(z_{T}) - Z_{G}I_{T}(z_{T})$   $Z_{RT}I_{T}(z_{T}) + Z_{RR}I_{R}(z_{R}) + Z_{RS1}I_{S1}(z_{S1}) + Z_{RS2}I_{S2}(z_{S2}) = V_{R}(z_{R}) = -Z_{R}I_{R}(z_{R})$   $Z_{S1T}I_{T}(z_{T}) + Z_{S1R}I_{R}(z_{R}) + Z_{S1S1}I_{S1}(z_{S1}) + Z_{S1S2}I_{S2}(z_{S2}) = V_{S1}(z_{S1}) = -Z_{S1}I_{S1}(z_{S1})$   $Z_{S2T}I_{T}(z_{T}) + Z_{S2R}I_{R}(z_{R}) + Z_{S2S1}I_{S1}(z_{S1}) + Z_{S2S2}I_{S2}(z_{S2}) = V_{S1}(z_{S1}) = -Z_{S2}I_{S2}(z_{S2})$ 

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# Mutual Coupling: E2E Modeling

# $\Box \text{ A system of linear equations (2 RIS elements for simplicity)}$ $Z_{TT}I_{T}(z_{T}) + Z_{TR}I_{R}(z_{R}) + Z_{TS1}I_{S1}(z_{S1}) + Z_{TS2}I_{S2}(z_{S2}) = V_{T}(z_{T}) = V_{G}(z_{T}) - Z_{G}I_{T}(z_{T})$ $Z_{RT}I_{T}(z_{T}) + Z_{RR}I_{R}(z_{R}) + Z_{RS1}I_{S1}(z_{S1}) + Z_{RS2}I_{S2}(z_{S2}) = V_{R}(z_{R}) = -Z_{R}I_{R}(z_{R})$ $Z_{S1T}I_{T}(z_{T}) + Z_{S1R}I_{R}(z_{R}) + Z_{S1S1}I_{S1}(z_{S1}) + Z_{S1S2}I_{S2}(z_{S2}) = V_{S1}(z_{S1}) = -Z_{S1}I_{S1}(z_{S1})$ $Z_{S2T}I_{T}(z_{T}) + Z_{S2R}I_{R}(z_{R}) + Z_{S2S1}I_{S1}(z_{S1}) + Z_{S2S2}I_{S2}(z_{S2}) = V_{S1}(z_{S1}) = -Z_{S2}I_{S2}(z_{S2})$



#### □ E2E channel

$$H_{e2e}(Z_{S1}, Z_{S2}) = \frac{V_L}{V_G}$$

 $=\frac{1}{\left(Z_{G}+Z_{TT}+\Psi_{TT}\left(Z_{S1},Z_{S2}\right)\right)\left(Z_{RT}+\Psi_{RT}\left(Z_{S1},Z_{S2}\right)\right)^{-1}\left(Z_{L}^{-1}\left(Z_{RR}+\Psi_{RR}\left(Z_{S1},Z_{S2}\right)\right)+1\right)-Z_{L}^{-1}\left(Z_{TR}+\Psi_{TR}\left(Z_{S1},Z_{S2}\right)\right)}$ 

# Mutual Coupling: E2E Modeling

**Theorem 1:** Let  $\mathcal{Z}_{XY}$  be the  $N_x \times N_y$  matrix whose (x, y)th entry is the mutual impedance between the xth and yth radiating elements of X and Y, where  $X, Y = \{T, S, R\}$  and  $N_x, N_y = \{N_t, N_{ris}, N_r\}$ , and T, S, R identify the transmitter, the RIS, and the receiver, respectively.  $\mathcal{H}_{E2E}$  is as follows:

$$\begin{aligned} \boldsymbol{\mathcal{H}}_{\text{E2E}} &= \left( \mathbf{I}_{N_{\text{r}} \times N_{\text{r}}} + \boldsymbol{\mathcal{P}}_{\text{RSR}} \mathbf{Z}_{\text{L}}^{-1} - \boldsymbol{\mathcal{P}}_{\text{RST}} \boldsymbol{\mathcal{P}}_{\text{GTST}}^{-1} \boldsymbol{\mathcal{P}}_{\text{TSR}} \mathbf{Z}_{\text{L}}^{-1} \right)^{-1} \\ &\times \boldsymbol{\mathcal{P}}_{\text{RST}} \boldsymbol{\mathcal{P}}_{\text{GTST}}^{-1} \end{aligned}$$

where  $\mathbf{I}_{N_{r} \times N_{r}}$  denotes an  $N_{r} \times N_{r}$  identity matrix,  $\mathbf{Z}_{G}$  is the  $N_{t} \times N_{t}$  diagonal matrix whose (t, t)th entry is  $Z_{Gt}$ ,  $\mathbf{Z}_{RIS}$  is the  $N_{ris} \times N_{ris}$  diagonal matrix whose (mn, mn)th entry is  $Z_{Smn}$ ,  $\mathbf{Z}_{L}$  is the  $N_{r} \times N_{r}$  diagonal matrix whose (r, r)th entry is  $Z_{Lr}$ ,  $\mathcal{P}_{GTST} = \mathbf{Z}_{G} + \mathcal{P}_{TST}$ , and:

$$\mathcal{P}_{XSY} = \mathcal{Z}_{XY} - \mathcal{Z}_{XS} (\mathbf{Z}_{RIS} + \mathcal{Z}_{SS})^{-1} \mathcal{Z}_{SY}$$

# Mutual Coupling: E2E Modeling

**Theorem 1:** Let  $\mathcal{Z}_{XY}$  be the  $N_x \times N_y$  matrix whose (x, y)th entry is the mutual impedance between the xth and yth radiating elements of X and Y, where  $X, Y = \{T, S, R\}$  and  $N_x, N_y = \{N_t, N_{ris}, N_r\}$ , and T, S, R identify the transmitter, the RIS, and the receiver, respectively.  $\mathcal{H}_{E2E}$  is as follows:

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ight)^{-1} \ & imes m{\mathcal{P}}_{\mathrm{RST}} m{\mathcal{P}}_{\mathrm{GTST}}^{-1} \end{split}$$



Modeling in the Presence of Scattering Objects (Multipath)







 $\mathbf{V}_{\mathrm{L}} = \mathcal{H}_{\mathrm{E2E}} \mathbf{V}_{\mathrm{G}}$ 





#### **Review The Discrete Dipole Approximation: A Review**

#### **Patrick Christian Chaumet**

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Abstract: There are many methods for rigorously calculating electromagnetic diffraction by objects of arbitrary shape and permittivity. In this article, we will detail the discrete dipole approximation (DDA) which belongs to the class of volume integral methods. Starting from Maxwell's equations, we will first present the principle of DDA as well as its theoretical and numerical aspects. Then, we will discuss the many developments that this method has undergone over time and the numerous applications that have been developed to transform DDA in a very versatile method. We conclude with a discussion of the strengths and weaknesses of the DDA and a description of the freely available DDA-based electromagnetic diffraction codes.

Keywords: electromagnetic simulation; DDA; numerical method; electromagnetic scattering





the properties of the dipoles (length, radius, etc.) and the load impedances depend on the material object being considered

$$\begin{split} \mathbf{H}_{\text{E2E}} &= \left(\mathbf{I}_{L} + \mathbf{Z}_{\text{RR}} \mathbf{Z}_{\text{L}}^{-1}\right)^{-1} \left[\mathbf{Z}_{\text{RT}} - \mathbf{Z}_{\text{RE}} \left(\mathbf{Z}_{\text{EE}} + \mathbf{Z}_{\text{SC}}\right)^{-1} \mathbf{Z}_{\text{ET}}\right] \\ &\times \left(\mathbf{Z}_{\text{TT}} + \mathbf{Z}_{\text{G}}\right)^{-1} \in \mathbb{C}^{L \times M} \end{split}$$

 $\mathbf{Z}_{\text{ET}}$  : Impedances between Tx and scatterers (RIS & objects)  $\mathbf{Z}_{\text{RE}}$  : Impedances between scatterers (RIS & objects) and Rx  $\mathbf{Z}_{\text{EE}}$  : Impedances between scatterers (RIS & objects)  $\mathbf{Z}_{\text{SC}}$  : Tunable loads of RIS and material impedances of scatterers

$$\mathbf{Z}_{\text{EE}} = \begin{bmatrix} \mathbf{Z}_{\text{OO}} & \mathbf{Z}_{\text{OS}} \\ \mathbf{Z}_{\text{SO}} & \mathbf{Z}_{\text{SS}} \end{bmatrix} \qquad \qquad \mathbf{Z}_{\text{SC}} = \begin{bmatrix} \mathbf{Z}_{\text{US}} & \mathbf{0}_{N_s \times N} \\ \mathbf{0}_{N \times N_s} & \mathbf{Z}_{\text{RIS}} \end{bmatrix}$$

$$\begin{split} \mathbf{H}_{\text{E2E}} &= \left(\mathbf{I}_{L} + \mathbf{Z}_{\text{RR}} \mathbf{Z}_{\text{L}}^{-1}\right)^{-1} \left[\mathbf{Z}_{\text{RT}} - \mathbf{Z}_{\text{RE}} \left(\mathbf{Z}_{\text{EE}} + \mathbf{Z}_{\text{SC}}\right)^{-1} \mathbf{Z}_{\text{ET}}\right] \\ &\times \left(\mathbf{Z}_{\text{TT}} + \mathbf{Z}_{\text{G}}\right)^{-1} \in \mathbb{C}^{L \times M} \end{split}$$



$$\mathbf{H}_{\text{E2E}} = \mathbf{Z}_{\text{RL}} \Big[ \mathbf{Z}_{\text{ROT}} - \mathbf{Z}_{\text{ROS}} \big( \mathbf{Z}_{\text{SS}} + \mathbf{Z}_{\text{SOS}} + \mathbf{Z}_{\text{RIS}} \big)^{-1} \mathbf{Z}_{\text{SOT}} \Big] \mathbf{Z}_{\text{TG}}$$

The obtained model is formally equivalent to free space:  $Z_{RIS}$  is decoupled from the matrices of mutual coupling

$$\begin{split} \mathbf{H}_{\text{E2E}} &= \left(\mathbf{I}_{L} + \mathbf{Z}_{\text{RR}} \mathbf{Z}_{\text{L}}^{-1}\right)^{-1} \left[\mathbf{Z}_{\text{RT}} - \mathbf{Z}_{\text{RE}} \left(\mathbf{Z}_{\text{EE}} + \mathbf{Z}_{\text{SC}}\right)^{-1} \mathbf{Z}_{\text{ET}}\right] \\ &\times \left(\mathbf{Z}_{\text{TT}} + \mathbf{Z}_{\text{G}}\right)^{-1} \in \mathbb{C}^{L \times M} \end{split}$$



$$\mathbf{H}_{\text{E2E}} = \mathbf{Z}_{\text{RL}} \Big[ \mathbf{Z}_{\text{ROT}} - \mathbf{Z}_{\text{ROS}} \big( \mathbf{Z}_{\text{SS}} + \mathbf{Z}_{\text{SOS}} + \mathbf{Z}_{\text{RIS}} \big)^{-1} \mathbf{Z}_{\text{SOT}} \Big] \mathbf{Z}_{\text{TG}}$$

Insights: The scatterers do not contribute as an additive term:  $H_{E2E} \neq H_{E2E}$  (free space) +  $H_{Multipath}$ 

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$$\mathbf{H}_{\text{E2E}} = \mathbf{Z}_{\text{RL}} \Big[ \mathbf{Z}_{\text{ROT}} - \mathbf{Z}_{\text{ROS}} \big( \mathbf{Z}_{\text{SS}} + \mathbf{Z}_{\text{SOS}} + \mathbf{Z}_{\text{RIS}} \big)^{-1} \mathbf{Z}_{\text{SOT}} \Big] \mathbf{Z}_{\text{TG}}$$

Insights: But, if  $Z_{SO} = 0$  and  $Z_{OS} = 0$ , then

$$\mathbf{H}_{\text{E2E}} = \mathbf{Z}_{\text{RL}} \Big[ \mathbf{Z}_{\text{RT}} - \mathbf{Z}_{\text{RO}} \overline{\mathbf{Z}}_{\text{OO}}^{-1} \mathbf{Z}_{\text{OT}} - \mathbf{Z}_{\text{RS}} \big( \mathbf{Z}_{\text{SS}} + \mathbf{Z}_{\text{RIS}} \big)^{-1} \mathbf{Z}_{\text{ST}} \Big] \mathbf{Z}_{\text{TG}}$$
<sup>49</sup>

$$\begin{split} \mathbf{H}_{\text{E2E}} &= \left(\mathbf{I}_{L} + \mathbf{Z}_{\text{RR}} \mathbf{Z}_{\text{L}}^{-1}\right)^{-1} \left[\mathbf{Z}_{\text{RT}} - \mathbf{Z}_{\text{RE}} \left(\mathbf{Z}_{\text{EE}} + \mathbf{Z}_{\text{SC}}\right)^{-1} \mathbf{Z}_{\text{ET}}\right] \\ &\times \left(\mathbf{Z}_{\text{TT}} + \mathbf{Z}_{\text{G}}\right)^{-1} \in \mathbb{C}^{L \times M} \end{split}$$



$$\mathbf{H}_{\text{E2E}} = \mathbf{Z}_{\text{RL}} \Big[ \mathbf{Z}_{\text{ROT}} - \mathbf{Z}_{\text{ROS}} \big( \mathbf{Z}_{\text{SS}} + \mathbf{Z}_{\text{SOS}} + \mathbf{Z}_{\text{RIS}} \big)^{-1} \mathbf{Z}_{\text{SOT}} \Big] \mathbf{Z}_{\text{TG}}$$

Insights: But, if  $Z_{SO} = 0$  and  $Z_{OS} = 0$ , then

 $\mathbf{H}_{E2E} = \mathbf{H}_{E2E} (\text{free space}) + \mathbf{H}_{\text{Multipath}}$ 

# Optimization

# **RIS:** A Loaded Thin Wire Model

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$$\begin{split} \mathbf{H}_{\mathrm{E2E}} &= \mathbf{Z}_{\mathrm{RL}} \left[ \mathbf{Z}_{\mathrm{ROT}} - \mathbf{Z}_{\mathrm{ROS}} \mathbf{Z}_{\mathrm{sca}} \mathbf{Z}_{\mathrm{SOT}} \right] \mathbf{Z}_{\mathrm{TG}} \\ \mathbf{Z}_{\mathrm{sca}} &= \left( \mathbf{Z}_{\mathrm{SS}} + \mathbf{Z}_{\mathrm{SOS}} + \mathbf{Z}_{\mathrm{RIS}} \right)^{-1} \end{split}$$

$$\begin{aligned} \mathbf{P0} & \max_{\mathbf{Q}, \mathbf{Z}_{\text{RIS}}} \log_2 \left[ \det \left( \mathbf{I}_L + \frac{\mathbf{H}_{\text{E2E}} \mathbf{Q} \mathbf{H}_{\text{E2E}}^H}{\sigma^2} \right) \right] \\ & \text{s.t.} & \text{Re} \{ \mathbf{Z}_{\text{RIS}}(k, k) \} = R_{0,k} \geq 0, \ \forall k \\ & \text{Im} \{ \mathbf{Z}_{\text{RIS}}(k, k) \} \in \mathcal{P}, \ \forall k \\ & \text{tr}(\mathbf{Q}) \leq P_t \\ & \mathbf{Q} \succcurlyeq \mathbf{0} \end{aligned}$$

By keeping  $\mathbf{Z}_{\text{RIS}}$  fixed, (P0) boils down to a conventional MIMO optimization problem. Specifically, let  $\mathbf{H}_{\text{E2E}} = \mathbf{U}_{\mathbf{H}_{\text{E2E}}} \mathbf{\Sigma}_{\mathbf{H}_{\text{E2E}}} \mathbf{V}_{\mathbf{H}_{\text{E2E}}}^{H}$  be the singular value decomposition of  $\mathbf{H}_{\text{E2E}}$ , where  $\mathbf{V}_{\mathbf{H}_{\text{E2E}}} \in \mathbb{C}^{M \times D}$ ,  $\mathbf{U}_{\mathbf{H}_{\text{E2E}}} \in \mathbb{C}^{L \times D}$ , and  $D = \text{rank}(\mathbf{H}_{\text{E2E}}) \leq \min(L, M)$ . Then, the optimal  $\mathbf{Q}^*$  is

$$\mathbf{Q}^{\star} = \mathbf{V}_{\mathbf{H}_{E2E}} \operatorname{diag}(p_1^{\star}, \dots, p_D^{\star}) \mathbf{V}_{\mathbf{H}_{E2E}}^H$$

where  $p_i^{\star} = \max\left(\left(1/\alpha - \sigma^2 / \Sigma_{\mathbf{H}_{E2E}}(i,i)^2\right), 0\right)$ , with  $\alpha$  satisfying  $\sum_{i=1}^{D} p_i^{\star} = P_t$  (water-filling power allocation).

By keeping Q fixed, the resulting optimization problem with respect to  $\mathbf{Z}_{\text{RIS}}$  simplifies to  $(k \in \{1, \ldots, N_{\text{RIS}}\})$ 

$$(\mathbf{P1}) \quad \max_{\mathbf{Z}_{\mathrm{RIS}}} \ \log_2 \left[ \det \left( \mathbf{I}_L + \frac{\mathbf{H}_{\mathrm{E2E}} \mathbf{Q} \mathbf{H}_{\mathrm{E2E}}^H}{\sigma^2} \right) \right]$$

s.t. 
$$\operatorname{Re}\{\mathbf{Z}_{\operatorname{RIS}}(k,k)\} = R_{0,k} \ge 0, \forall k$$
  
 $\operatorname{Im}\{\mathbf{Z}_{\operatorname{RIS}}(k,k)\} \in \mathcal{P}, \forall k$ 

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$$(\mathbf{P1}) \max_{\mathbf{Z}_{\mathrm{RIS}}} \log_2 \left[ \det \left( \mathbf{I}_L + \frac{\mathbf{H}_{\mathrm{E2E}} \mathbf{Q} \mathbf{H}_{\mathrm{E2E}}^H}{\sigma^2} \right) \right]$$
  
s.t.  $\mathrm{Re} \{ \mathbf{Z}_{\mathrm{RIS}}(k,k) \} = R_{0,k} \ge 0, \ \forall k$ 

 $\operatorname{Im}\{\mathbf{Z}_{\mathrm{RIS}}(k,k)\} \in \mathcal{P}, \forall k$ 

#### □ The approach consists of three steps:

- Sherman-Morrison's formula
- □ Sylvester's determinant theorem
- **Gram-Schmidt's orthogonalization process**

$$\mathbf{Z}_{\mathrm{sca}} = (\mathbf{Z}_{\mathrm{SS}} + \mathbf{Z}_{\mathrm{SOS}} + \mathbf{Z}_{\mathrm{RIS}})^{-1}$$

$$\mathbf{Z}_{\mathrm{sca}} = \left(\mathbf{Z}_{\mathrm{SS}} + \mathbf{Z}_{\mathrm{SOS}} + \mathbf{Z}_{\mathrm{RIS}}\right)^{-1}$$

$$\mathbf{Z}_{\text{sca}} = \left(\mathbf{Z}_{\text{SS}} + \mathbf{Z}_{\text{SOS}} + \mathbf{Z}_{\text{RIS},k} + \mathbf{Z}_{\text{RIS}}(k,k)\mathbf{e}_{k}\mathbf{e}_{k}^{T}\right)^{-1}$$

$$\mathbf{Z}_{\mathrm{sca}} = \left(\mathbf{Z}_{\mathrm{SS}} + \mathbf{Z}_{\mathrm{SOS}} + \mathbf{Z}_{\mathrm{RIS}}\right)^{-1}$$

$$\mathbf{Z}_{\text{sca}} = \left(\mathbf{Z}_{\text{SS}} + \mathbf{Z}_{\text{SOS}} + \mathbf{Z}_{\text{RIS},k} + \mathbf{Z}_{\text{RIS}}(k,k)\mathbf{e}_{k}\mathbf{e}_{k}^{T}\right)^{-1}$$



 $\mathbf{A}_k = \mathbf{Z}_{SS} + \mathbf{Z}_{SOS} + \mathbf{Z}_{RIS,k}, \quad z_k = \mathbf{Z}_{RIS}(k,k)$ 

- □ The approach consists of three steps:
  - □ Sherman-Morrison's formula
  - □ Sylvester's determinant theorem
  - **Gram-Schmidt's orthogonalization process**

$$\mathbf{Z}_{\text{sca}} = \mathbf{Z}_{\text{sca}} \left( z_k \right) = \mathbf{A}_k^{-1} - \frac{\mathbf{A}_k^{-1} \mathbf{e}_k \mathbf{e}_k^T \mathbf{A}_k^{-1}}{1 + z_k \mathbf{e}_k^T \mathbf{A}_k^{-1} \mathbf{e}_k} z_k$$

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□ The approach consists of three steps:

- Sherman-Morrison's formula
- □ Sylvester's determinant theorem
- **Gram-Schmidt's orthogonalization process**

$$R(z_k) = \log_2 \left[ \det \left( \mathbf{I}_L + \frac{\mathbf{B}_k \mathbf{Q} \mathbf{B}_k^H}{\sigma^2} \right) \right] + \log_2 \left[ \det(\mathbf{S}_k (z_k)) \right]$$
$$\mathbf{S}_k (z_k) = \mathbf{I}_L + \mathbf{U}_k \mathbf{\Sigma}_k^{-1} \mathbf{U}_k^H \left( \mathbf{X}_1 (z_k) + \mathbf{X}_2 (z_k) \right)$$
$$\mathbf{\bigcup}$$

 $\det(\mathbf{S}_{k}(z_{k})) = \det\left(\mathbf{I}_{L} + \boldsymbol{\Sigma}_{k}^{-\frac{1}{2}}\mathbf{U}_{k}^{H}\left(\mathbf{X}_{1}(z_{k}) + \mathbf{X}_{2}(z_{k})\right)\mathbf{U}_{k}\boldsymbol{\Sigma}_{k}^{-\frac{1}{2}}\right)$ 

□ The approach consists of three steps:

- Sherman-Morrison's formula
- □ Sylvester's determinant theorem
- **Gram-Schmidt's orthogonalization process**

$$\begin{split} \mathbf{S}_{k}\left(z_{k}\right) &= \mathbf{I}_{L} + \frac{\tilde{\mathbf{u}}_{k}\tilde{\mathbf{v}}_{k}^{H}}{\sigma^{2}\chi_{k}\left(z_{k}\right)} + \frac{\tilde{\mathbf{v}}_{k}\tilde{\mathbf{u}}_{k}^{H}}{\sigma^{2}\chi_{k}^{*}\left(z_{k}\right)} + \frac{\tilde{\mathbf{u}}_{k}\tilde{\mathbf{u}}_{k}^{H}\mathbf{v}_{k}^{H}\mathbf{Q}\mathbf{v}_{k}}{\sigma^{2}|\chi_{k}\left(z_{k}\right)|^{2}}\\ \tilde{\mathbf{u}}_{k} &= \mathbf{\Sigma}_{k}^{-\frac{1}{2}}\mathbf{U}_{k}^{H}\mathbf{u}_{k}, \quad \tilde{\mathbf{v}}_{k}^{H} = \mathbf{v}_{k}^{H}\mathbf{Q}\mathbf{B}_{k}^{H}\mathbf{U}_{k}\mathbf{\Sigma}_{k}^{-\frac{1}{2}} \end{split}$$

The vectors  $u_k$  and  $v_k$  are not orthogonal  $\rightarrow$  orthogonalization

$$\begin{split} \mathbf{t}_1 &= \frac{1}{||\tilde{\mathbf{u}}_k||} \tilde{\mathbf{u}}_k, \quad \mathbf{t}_2 = \frac{1}{||\mathbf{t}||} \mathbf{t} \\ \mathbf{t} &= \tilde{\mathbf{v}}_k - \frac{\langle \tilde{\mathbf{v}}_k, \mathbf{t}_1 \rangle}{\langle \mathbf{t}_1, \mathbf{t}_1 \rangle} \mathbf{t}_1 = \frac{||\tilde{\mathbf{u}}_k||^2 \tilde{\mathbf{v}}_k - \tilde{\mathbf{u}}_k^H \tilde{\mathbf{v}}_k \tilde{\mathbf{u}}_k}{||\tilde{\mathbf{u}}_k||^2} \end{split}$$

□ The approach consists of three steps:

- Sherman-Morrison's formula
- □ Sylvester's determinant theorem
- **Gram-Schmidt's orthogonalization process**

$$\det(\mathbf{S}_{k}) = \det\left( (\mathbf{t}_{1} \ \mathbf{t}_{2}) \begin{pmatrix} 1 + s_{k} (z_{k}) & \frac{||\tilde{\mathbf{u}}_{k}||\tilde{\mathbf{v}}_{k}^{H}\mathbf{t}_{2}}{\sigma^{2}\chi_{k}(z_{k})} \\ \frac{||\tilde{\mathbf{u}}_{k}||\mathbf{t}_{2}^{H}\tilde{\mathbf{v}}_{k}}{\sigma^{2}\chi_{k}^{*}(z_{k})} & 1 \end{pmatrix} \begin{pmatrix} \mathbf{t}_{1}^{H} \\ \mathbf{t}_{2}^{H} \end{pmatrix} \right)$$
$$= \det\left( \begin{pmatrix} 1 + s_{k} (z_{k}) & \frac{||\tilde{\mathbf{u}}_{k}||\tilde{\mathbf{v}}_{k}^{H}\mathbf{t}_{2}}{\sigma^{2}\chi_{k}(z_{k})} \\ \frac{||\tilde{\mathbf{u}}_{k}||\mathbf{t}_{2}^{H}\tilde{\mathbf{v}}_{k}}{\sigma^{2}\chi_{k}^{*}(z_{k})} & 1 \end{pmatrix} \right) = \det(\mathbf{W})$$

$$s_k(z_k) = \frac{\|\tilde{\mathbf{u}}_k\| \tilde{\mathbf{v}}_k^H \mathbf{t}_1}{\sigma^2 \chi_k(z_k)} + \frac{\|\tilde{\mathbf{u}}_k\| \mathbf{t}_1^H \tilde{\mathbf{v}}_k}{\sigma^2 \chi_k^*(z_k)} + \frac{\|\tilde{\mathbf{u}}_k\|^2 \mathbf{v}_k^H \mathbf{Q} \mathbf{v}_k}{\sigma^2 |\chi_k(z_k)|^2}$$

Since  $\mathbf{W} = \mathbf{W}(z_k)$  is a 2×2 matrix, the determinant of  $\mathbf{S}_k = \mathbf{S}_k(z_k)$  can be expressed in closed-form as

$$\det(\mathbf{S}_k(z_k)) = 1 + \frac{c_1}{\chi_k(z_k)} + \frac{c_1^*}{\chi_k^*(z_k)} + \frac{c_2}{|\chi_k(z_k)|^2}$$

where

$$c_1 = \frac{||\tilde{\mathbf{u}}_k||\tilde{\mathbf{v}}_k^H \mathbf{t}_1}{\sigma^2}, \ c_2 = \frac{||\tilde{\mathbf{u}}_k||^2 \mathbf{v}_k^H \mathbf{Q} \mathbf{v}_k}{\sigma^2} - \frac{||\tilde{\mathbf{u}}_k||^2 |\tilde{\mathbf{v}}_k^H \mathbf{t}_2|^2}{\sigma^4}$$

In conclusion, since  $\chi_k(z_k) = 1 + a_k z_k$ , with  $z_k = R_{0,k} + jX_k$  and  $R_{0,k}$  is assumed known and fixed, (P1) boils down to maximizing the single-variable (i.e.,  $X_k$ ) function

$$f(X_k) = 1 + \frac{c_1}{1 + a_k(R_{0,k} + jX_k)} + \frac{c_1^*}{1 + a_k^*(R_{0,k} + jX_k)^*} + \frac{c_2}{|1 + a_k(R_{0,k} + jX_k)|^2}, \quad X_k \in \mathcal{P}$$

# Algorithm 1 Proposed algorithm for solving (P0)

**Input**: Compute the impedance matrices from [4, Lemma 2]; Initialize:  $q = 0, \epsilon \geq 0, \mathbf{r}_0 = [R_{0,1}, \dots, R_{0,N_{\text{RIS}}}]^T, \mathbf{x}^{(0)} =$  $[X_1^{(0)}, \dots, X_{N_{\text{DIG}}}^{(0)}]^T \in \mathcal{P}^{N_{\text{RIS}}}, R^{(-1)} = 0, R^{(0)} = R(\mathbf{Q}^{(0)}, \mathbf{Z}^{(0)})$ with  $\mathbf{Z}^{(0)} = \operatorname{diag}(\mathbf{r}_0) + j \operatorname{diag}(\mathbf{x}^{(0)})$  and  $R(\cdot, \cdot)$  defined in (8); while  $|R^{(q)} - R^{(q-1)}| > \epsilon$  do Compute  $\mathbf{Q}^{\star}$  from (14); for  $k = 1, \ldots, N_{\text{RIS}}$  do Compute  $X_k^{\star}$  from Proposition 1; Update  $\mathbf{Z}_{\text{RIS}}^{\star}(k,k) \leftarrow R_{0,k} + jX_k^{\star};$ end for  $q = q + 1, R^{(q)} = R(\mathbf{Q}^{\star}, \mathbf{Z}_{BIS}^{\star});$ end while **Return**:  $\mathbf{Q}^*$  and  $\mathbf{Z}^*_{\text{BIS}}$ .

# Numerical Examples



# **Optimization in Free Space (SISO, Fixed Size RIS)**



# **Optimization in Free Space (SISO, Fixed Size RIS)**



# **Optimization in Free Space (SISO, Fixed Size RIS)**



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# **Optimization in Free Space**

# Multi-User MIMO



# **Optimization in Free Space (MIMO, Fixed Size RIS)**


## **Optimization in Free Space (MIMO, Fixed Size RIS)**



## **MIMO-RIS Optimization with Scattering Objects**



## MIMO-RIS Optimization with Scattering Objects



## MIMO-RIS Optimization with Scattering Objects

Table II: Comparison of the execution time [seconds]

d	Algo. 1 (90%)	[8]	]	d	Algo. 1 (98%)	[9]
$\lambda/2$	0.001	0.800		$\lambda/2$	0.001	0.0154
$\lambda/4$	0.004	0.770	1	$\lambda/4$	0.008	0.896
$\lambda/8$	0.167	8.135		$\lambda/8$	0.834	27.686
$\lambda/16$	16.530	213.128		$\lambda/16$	170.807	946.404

## Conclusion: Approach to Model the Near Field

- Paradigm #1: The wavefronts of the electromagnetic waves are (approximated as) locally planar on the antenna arrays
  - RISs/HoloS are electrically large and the transmission distances are shrinking



## Conclusion: Approach to Model the Mutual Coupling

- Paradigm #2: The radiating elements of antenna-arrays are decoupled electromagnetically
  - □ The inter-distances are smaller than the wavelength ( $< \lambda/2$ )





#### Programmable Metasurfaces for Wireless Communications: A Loaded Thin Wire Model

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